

Class: SE

ZEAL EDUCATION SOCIETY'S ZEAL COLLEGE OF ENGINEERING AND RESEARCH NARHE | PUNE -41 | INDIA

Record No.: ZCOER-ACAD/R/16H

Revision: 00

Date:01/04/2021

Unit Wise Real Time Applications/Live Examples

Department: Mechanical

Semester: I Div.: A &B Academic Year: 2024–2025

Course: Solid Mechanics





Record No.: ZCOER-ACAD/R/16H

Revision: 00

Unit No Name	Real life Applications			
	Engage: Take your iPod into class and dangle it by the earphone cable. Cut open the cable on an old			
	set of earphones to expose cable and insulation			
	Explore: Pass around class lengths of copper wire and lengths of empty hollow insulation and invite students to stretch them. Discuss relative extensions and stiffness. Someone will probably snap one so talk about ultimate tensile stress. Be sure have to enough lengths that every student has at least one to play with while you are talking.			
	Tensile Force Compression Force			
	Temperature stress			



Record No.: ZCOER-ACAD/R/16H

Revision: 00

Date:01/04/2021

Unit No Name	Real life Applications



25

Record No.: ZCOER-ACAD/R/16H

Revision: 00

Unit NoName	Real life Applications
	Bending moments and shear stress diagrams for skate board
	Engage:
	Ride a skateboard into class. Explore:
Unit II: SFD & BMD	Discuss the shear forces and bending moment's set-up in the skateboard when you stand on it sideways balanced on your heels, i.e. approximating a point load. When you stand of the board more normally, how do the shear forces and bending moments change? Discuss where you need to stand to induce a zero bending moment.
	Explain: Plot the shear force and bending moment diagrams for the case where you were rocking
	on your heels. P
	A B Resolve vertically: $R_A + R_B = P$
	$\longleftarrow \qquad L \longrightarrow \qquad \qquad \text{Moments about A:} \qquad Pa - R_B L = 0$
	R_A R_B Thus: $R_A = \frac{Pb}{T}$ $R_B = \frac{Pa}{T}$
	$\begin{array}{c} \leftarrow x \longrightarrow \\ Resolve vertically: F = R = \frac{Pb}{\sqrt{r}} \end{array}$
	$A \models P \qquad Moments: M = R x = \frac{Pbx}{m}$
	F Considering the cut section (a <x<l)< td=""></x<l)<>
	$\begin{array}{c} & & \\ \hline R_{E} \end{array} \end{array}$ Resolve vertically: $\begin{array}{c} P_{U} \\ P_{U} \\ P_{U} \end{array}$
	$F = R_{A} - P = -$
	$M \qquad Bab \qquad Moments: = -(-) = -(-)$ $M \qquad R_A x \qquad P x \qquad a \qquad L \qquad x$
	L X





Record No.: ZCOER-ACAD/R/16H		Revision: 00	Date:01/04/2021
Unit NoName		Real life Applic	ations
	Elaborate: When a skateboarder bending moment is a	crosses a plank we can maximum. The situation $A \xrightarrow{P}$ $A \xrightarrow{P}$ $L \xrightarrow{L}$	determine the position at which the can be idealized as shown below:
	The shear force and be small sections of beam	ending moment diagrams ca , i.e.	in be plotted as previously considering
	Taking moments about $R_A L - \frac{P}{2}(L - x)$ Thus, $R_A = \frac{P}{L}(x)$ For $(s < x)$ Resolving verting Taking moments For $(x < s < (a + x))$ Resolving verting Taking moments	a B gives: $f(x) - a - \frac{P}{2}(L - x) = 0$ $f(L - x - \frac{a}{2}) \qquad M$ $f(x) = \frac{A}{R_A} \qquad F$ cally: $F = -R_A$ ts: $M = -R_A s$ $f(x) = \frac{P}{2} - R_A$ ts: $M = \frac{P}{2} - R_A$ ts: $M = \frac{P}{2}(s - x) - R_A s$	P/2 P/2
	For $(s > (a + x))$ Resolving verti Taking momen M = P($A \xrightarrow{P/2} P/2 \xrightarrow{P/2} M$ $A \xrightarrow{F} S \xrightarrow{F} F$ R_A cally: $F = P - R_A$ ts: $\left(s - x - \frac{a}{2}\right) - R_A s$	N.B. These diagrams have been plotted assuming that $(x + a/2) > L/2$, if this were not the case then the diagrams would look slight different. The symmetry of the situation allows only this case to be considered. There are two places where M_c occurs that are symmetric about the mid-point of the beam.



Record No.: ZCOER-ACAD/R/16H Revision: 00 Date:01/04/2021 Unit No. -Name **Real life Applications** For maximum M_C : $\frac{\partial M_c}{\partial x} = 0$ and $M_c = R_A x = \frac{Px}{2L} (2L - 2x - a)$ So, $\frac{\partial M_C}{\partial x} = 2L - 4x - a = 0$ and $x = \frac{L}{2} - \frac{a}{4}$ Thus, $\hat{M}_{C} = \frac{P}{2L} \left(2L - 2\left(\frac{L}{2} - \frac{a}{4}\right) - a \right) \left(\frac{L}{2} - \frac{a}{4}\right) = \frac{P}{16L} (2L - a)^{2}$ So for a 1.8m plank and typical skate board (a=65cm) carrying a 65kg person, $\hat{M}_{c} = \frac{65 \times 9.81}{16 \times 3} (3.6 - 0.65)^{2} = 116 \text{ Nm}$ If the plank is 13cm wide and 1.8cm thick, then the maximum bending stress is $\sigma = \frac{\hat{M}_{C}y}{I} = \frac{\hat{M}_{C}(h/2)}{(bh^{3}/12)} = \frac{6 \times 116}{0.13 \times 0.018^{2}} = 16.5 \text{ MPa}$ This compares to compressive ultimate strengths for common woods in the range 35 to 55 MPa parallel to the grain and 4 to 10MPa perpendicular to the grain. Bending moments and shear stress diagrams for weight lifter 100 lbs 100 lbs 30 lbs 50 lbs 50 lbs 70 lbs



Record No.: ZCOER-ACAD/R/16H

Revision: 00





Record No.: ZCOER-ACAD/R/16H

Revision: **00**

Date:01/04/2021





Record No.: ZCOER-ACAD/R/16H

Revision: 00





Record No.: ZCOER-ACAD/R/16H

Revision: 00

Date:01/04/2021

Unit No. -Name	Real life Applications
	Explain:
	Work through the example below:
	Ultimate strength in shear for aluminum alloy is 240MN/m ² . So, to release the cap we need to achieve this stress level in the closure.
	Shear stress due to torsion, $\tau = \frac{Tr}{J}$
	where T is applied torque, r is the radius at which the shear stress occurs and J is the second polar moment of area, " $J = \pi R^4/2$ " and for a thin-walled tube is approximated by $J = 2\pi R^3 t$, where R is wall radius and t the wall thickness. Thus the torque required to open the bottle when $R = 1.2$ cm and $t = 0.1$ mm;
	$T = 2\pi R^2 t \tau = 2\pi \times 0.012^2 \times 0.0001 \times (240 \times 10^6) = 22 \mathrm{Nm}$
	This is about three times the average hand-grip torque strength of an $adult^4$. Perforations imply that the load bearing area is reduced by about a quarter thus reducing the torque required to $=22/4=5.5$ Nm.
	Elaborate
	Consider the effect of the torque on the glass neck of the bottle, if the thickness of the glass is 3mm:
	$\tau = \frac{Tr}{J} = \frac{5.5 \times 0.012}{\pi (0.024^4 - 0.018^4)/32} = 3.0 \mathrm{MPa}$
	Since the mean strength of soda glass is about 65MPa there is no danger of failure even allowing for a stress concentration of three in the threads of the bottle, i.e. $\tau_{max} = \tau \times SCF = 9$ MPa. Now if the cap is damaged by a dent then it may jam and a strong person could exert three times the typical torque for an adult, i.e. about 22N then $\tau = 36$ MPa (including the stress concentration) – still no problem.
	However, if the thread on the bottle is mis-formed so that the wall thickness is reduced by 1mm and the cap is damaged and a strong adult attempts to open the bottle, then
	$\tau_{\text{max}} = \frac{Tr}{J} \times SCF = \frac{22 \times 0.012}{\pi (0.022^4 - 0.018^4)/32} \times 3 = 62.4 \text{ MPa}$
	Failure is likely! This simplistic analysis ignores the presence of cracks etc. and instead focuses on using the torsion stress-strain relationships.



Record No.: ZCOER-ACAD/R/16H

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Revision: 00

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	Explain: Ask the students, working in pairs and sketching, to identify forces and moments acting about the center of the cross-section of the pole that are equivalent to the weight of a player hanging on the rim (<i>solid arrow</i>). The solution is a compressive force and a moment (<i>dashed arrows</i>).
	Explain that if these two forces only produce linear elastic deformation then their effects can be added together, or superimposed. Discuss principle of superposition. $ \frac{P}{\frac{1}{1+1+1+1+1+1+1+1+1+1+1+1+1+1+1+1+1+1+$
	Elaborate
	For a pole 10cm square manufactured from aluminum with a 60cm offset when a player hangs from the front of the ring at an effective distance from the backboard of 50cm, the maximum tensile stress in the pole occurs on the back of the pole:
	Maximum tensile stress = Maximum bending stress - compressive stress
	$\sigma_{\max} = \frac{M(h/2)}{I} - \frac{P}{bh} = \frac{(Pe)h/2}{bh^3/12} - \frac{P}{bh} = \frac{6(Pe)}{bh^2} - \frac{P}{bh}$
	So, for a 90kg player, ignoring the mass of the backboard etc.
	$\sigma_{\max} = \frac{6(90 \times 9.81 \times [60 + 50] \times 10^{-2})}{(10 \times 10^{-2})^3} - \frac{90 \times 9.81}{(10 \times 10^{-2})^2} = 5827140 + 88290 = 5.9 \text{ MPa}$



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